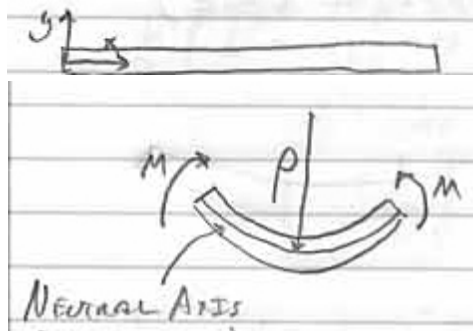


2.001 - MECHANICS AND MATERIALS I
 Lecture #21
 11/21/2006
 Prof. Carol Livermore

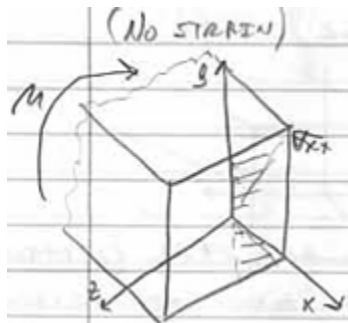
Recall from last time:
 Beam Bending



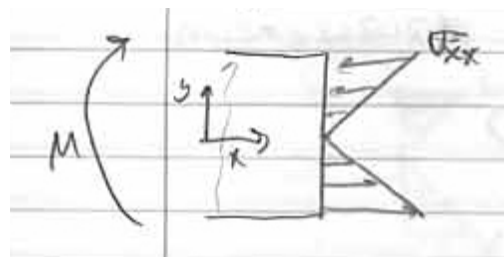
$y = 0$ on neutral axis
 $\epsilon_{xx} = \frac{-y}{\rho}$ (Note: purely geometric, no material properties)
 $\sigma_{xx} = \epsilon_{xx}E$ (All other σ are equal to 0)

So:

$$\sigma_{xx} = \frac{-Ey}{\rho}$$



Force Equilibrium:



$$\sum F_x = 0$$

$$\int_A \sigma_{xx} dA = 0$$

$$\int_A \frac{Ey}{\rho} dA = 0$$

If E is constant in y then $\int_A y dA = 0$.

Moment Equilibrium

$$\sum M_z = 0$$

$$M = - \int_A \sigma_{xx} y dA$$

$$M = \int_A \frac{Ey^2}{\rho} dA$$

Special case: E constant:

$$M = \frac{1}{\rho} EI$$

$$I = \int_A y^2 dA$$

New this time:

Recall:

$$\sigma_{xx} = \frac{-Ey}{\rho}$$

For constant E (special case):

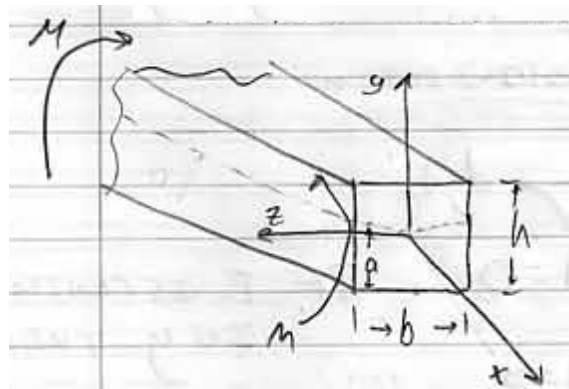
$$M = \frac{EI}{\rho}$$

So:

$$\frac{E}{\rho} = \frac{M}{I} = \frac{-\sigma_{xx}}{y}$$

$$\sigma_{xx} = \frac{-My}{I}$$

EXAMPLE: Find location of neutral axis for rectangular beam



E is constant across cross-section. Recall force equilibrium.

$$\int_A \frac{E y}{\rho} dA = 0$$

$$\frac{E}{\rho} \int_A y dA = 0$$

$$\frac{E}{\rho} \int_{-\frac{b}{2}}^{\frac{b}{2}} \int_a^{h-a} y dy dz = 0$$

$$\int_{-\frac{b}{2}}^{\frac{b}{2}} \left[\frac{y^2}{2} \right]_a^{h-a} dz = 0$$

$$\frac{1}{2} \int_{-\frac{b}{2}}^{\frac{b}{2}} [(h-a)^2 - a^2] dz = 0$$

$$\frac{1}{2} \int_{-\frac{b}{2}}^{\frac{b}{2}} (h^2 - 2ha) dz = 0$$

$$\frac{1}{2} \left[(h^2 - 2ha)z \right]_{-\frac{b}{2}}^{\frac{b}{2}} = 0$$

$$\frac{1}{2} (h^2 - 2ha) \left(\frac{b}{2} + \frac{b}{2} \right) = 0$$

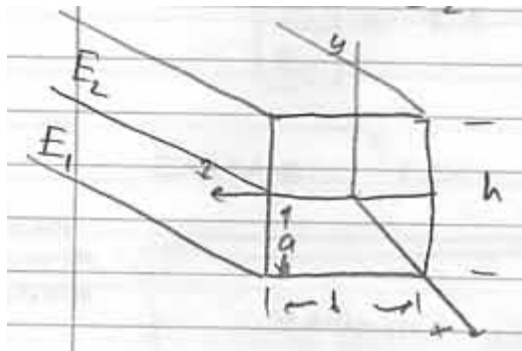
$$\frac{b}{2} (h^2 - 2ha) = 0$$

$$h^2 = 2ha$$

$$a = \frac{h}{2}$$

So the neutral axis is in the center of the beam.

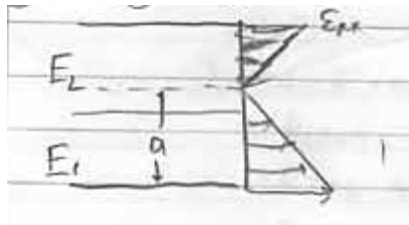
What if $E_2 > E_1$ in:



a is the distance to neutral axis.

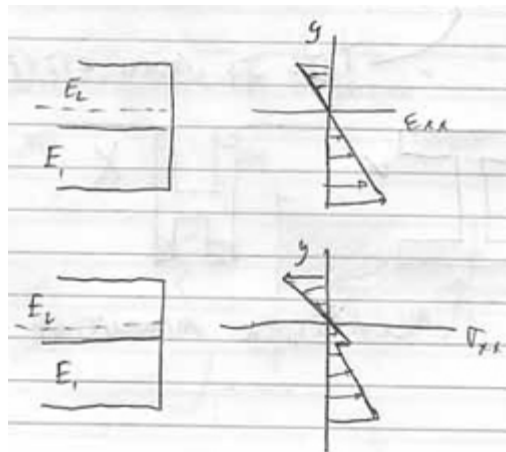
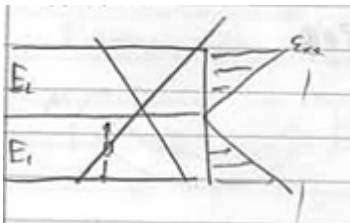
$$\int_A \frac{E y}{\rho} dA = 0$$

$$\frac{1}{\rho} \int_A E(y) y dA = 0$$

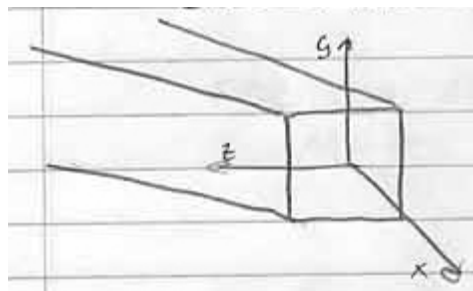


$$\int_{-\frac{b}{2}}^{\frac{b}{2}} \left[\int_{-a}^{-a+\frac{b}{2}} E_1 y dy + \int_{-a+\frac{b}{2}}^{h-a} E_2 y dy \right] dz = 0$$

Note:



Example: Moment of Inertia
One material rectangular beam



$$I = \int_A y^2 dA$$

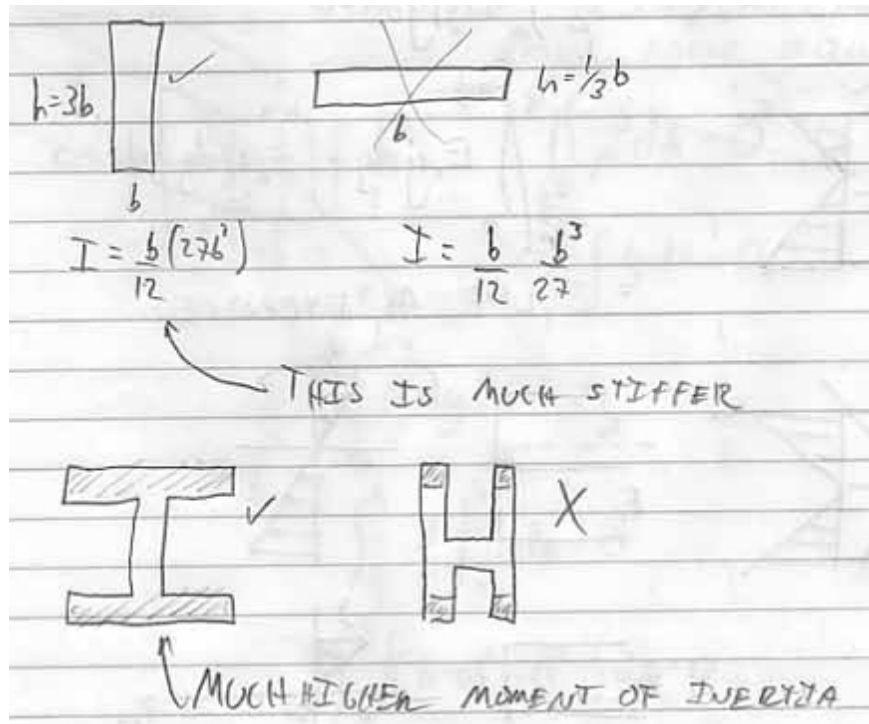
$$I = \int_{-\frac{b}{2}}^{\frac{b}{2}} dz \int_{-\frac{h}{2}}^{\frac{h}{2}} y^2 dy$$

$$I = \int_{-\frac{b}{2}}^{\frac{b}{2}} dz \left[\frac{y^3}{3} \right]_{-\frac{h}{2}}^{\frac{h}{2}}$$

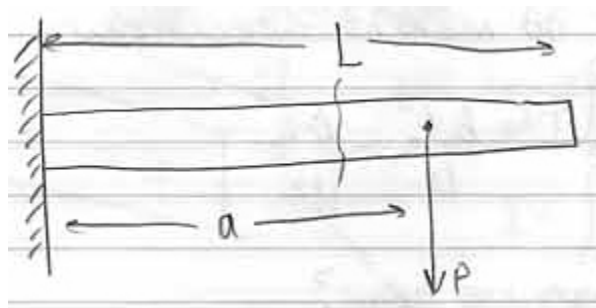
$$I = \int_{-\frac{b}{2}}^{\frac{b}{2}} dz \frac{h^3}{12}$$

$$I = \frac{bh^3}{12}$$

Beam Design

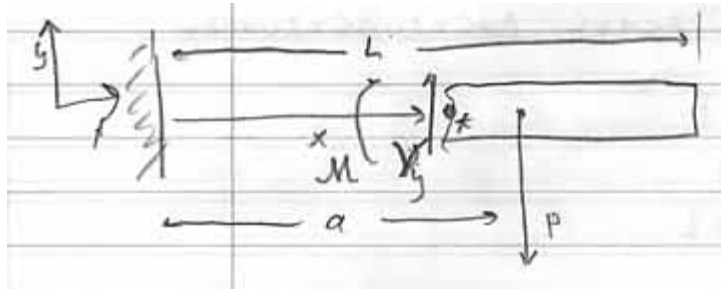


Example:



Find σ_{xx} .

FBD:



$$\sum F_y = 0$$

$$V_y - P = 0$$

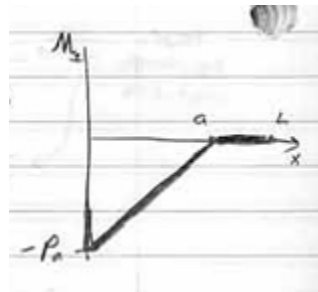
$$V_y = P$$

$$\sum M_x = 0$$

$$-M_z - P(a - x) = 0$$

$$M_z = -P(a - x) = 0$$

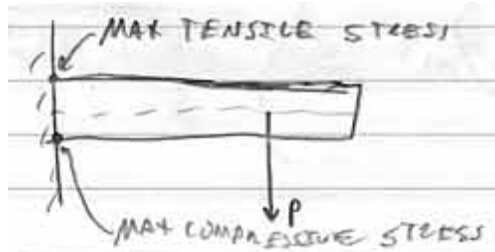
$$\frac{1}{\rho} = \frac{M_z(x)}{EI}$$



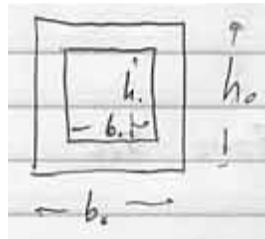
What about shear?

Distortion of planar sections of beam. This can be ignored for slender (long and skinny beams)

$$\sigma_{xx} = \frac{-My}{I} = \frac{-M_z(x)y}{I} = \frac{P(a-x)y}{I}$$



$$\sigma_{xx_{max}} = \frac{Pa \frac{h}{2}}{\frac{1}{12}bh^3} = \frac{6Pa}{bh^2}$$



Solve for I

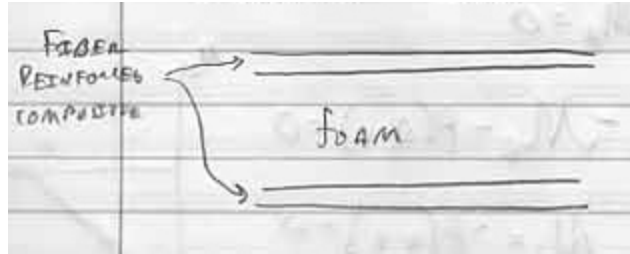
a. Do areas of integration

b. $I = \frac{b_0 h_0^3}{12} - \frac{b_i h_i^3}{12}$

What about a composite beam? This does not work because E was taken out of integral during derivation.

$$\begin{bmatrix} E_2 \\ E_1 \end{bmatrix} = "EI" \int_A E_y dA$$

Example: Skis



Get good stiffness (bending) but give up axial stiffness and lower weight.

Other examples:

- Plants
- Bird bones
- Airplanes

Recall, x-axis is all for "pure bending"

