

2.43 ADVANCED THERMODYNAMICS

Spring Term 2024

LECTURE 12

Room 3-442

Friday, March 15, 11:00am - 1:00pm

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Room 3-351d

**Stable-equilibrium properties of
MIXTURES
(within the simple-system model)**

**Partial properties
Gibbs-Dalton ideal mixtures
Mixing and separation
Osmotic pressure and blue energy
Stratification**

Partial properties from the chemical potentials

$$G = E - TS + pV = G(T, p, \mathbf{n}) \quad dG = -S dT + V dp + \boldsymbol{\mu} \cdot d\mathbf{n}$$

$$\left(\frac{\partial G}{\partial T}\right)_{T,p,\mathbf{n}} = -S(T, p, \mathbf{n}) \quad \left(\frac{\partial G}{\partial p}\right)_{T,p,\mathbf{n}} = V(T, p, \mathbf{n}) \quad \mu_i = \left(\frac{\partial G}{\partial n_i}\right)_{T,p,\mathbf{n}'_i} = \mu_i(T, p, \mathbf{n}\mathbf{y})$$

$$d\mu_i = \underbrace{\left(\frac{\partial \mu_i}{\partial T}\right)_{p,\mathbf{n}}}_{-s_i} dT + \underbrace{\left(\frac{\partial \mu_i}{\partial p}\right)_{T,\mathbf{n}}}_{v_i} dp + \sum_{j=1}^r \underbrace{\left(\frac{\partial \mu_i}{\partial n_j}\right)_{T,p,\mathbf{n}'_j}}_{\mu_{i,j} = \mu_{i,j}} dn_j = -s_i dT + \underbrace{v_i dp + \sum_{j=1}^r \mu_{i,j} dn_j}_{d\mu_i|_T}$$

where we define

$$-\left(\frac{\partial \mu_i}{\partial T}\right)_{p,\mathbf{n}} = -\left(\frac{\partial^2 G}{\partial T \partial n_i}\right)_{p,\mathbf{n}'_i} = \left(\frac{\partial S}{\partial n_i}\right)_{T,p,\mathbf{n}'_i} = s_i(T, p, \mathbf{n}\mathbf{y}) \quad \text{Partial entropy of constituent } i$$

$$\left(\frac{\partial \mu_i}{\partial p}\right)_{T,\mathbf{n}} = \left(\frac{\partial^2 G}{\partial p \partial n_i}\right)_{T,\mathbf{n}'_i} = \left(\frac{\partial V}{\partial n_i}\right)_{T,p,\mathbf{n}'_i} = v_i(T, p, \mathbf{n}\mathbf{y}) \quad \text{Partial volume of constituent } i$$

$$\left(\frac{\partial \mu_i}{\partial n_j}\right)_{T,p,\mathbf{n}'_j} = \left(\frac{\partial^2 G}{\partial n_j \partial n_i}\right)_{T,p,\mathbf{n}'_{ij}} = \left(\frac{\partial \mu_j}{\partial n_i}\right)_{T,p,\mathbf{n}'_{ij}} = \mu_{i,j}(T, p, \mathbf{n}\mathbf{y}) = \mu_{j,i}(T, p, \mathbf{n}\mathbf{y})$$

notice that, from $dE = T dS - p dV + \boldsymbol{\mu} \cdot d\mathbf{n}$ and $dH = T dS + V dp + \boldsymbol{\mu} \cdot d\mathbf{n}$ we also have

$$\left(\frac{\partial E}{\partial n_i}\right)_{T,p,\mathbf{n}'_i} = e_i(T, p, \mathbf{n}\mathbf{y}) = T s_i - p v_i + \mu_i \quad \text{Partial energy of constituent } i$$

$$\left(\frac{\partial H}{\partial n_i}\right)_{T,p,\mathbf{n}'_i} = h_i(T, p, \mathbf{n}\mathbf{y}) = T s_i + \mu_i = \left(\frac{\partial(\mu_i/T)}{\partial(1/T)}\right)_{p,\mathbf{n}} \quad \text{Partial enthalpy of constituent } i$$

All partial properties can be evaluated once we know the chemical potentials as functions of T , p , \mathbf{y} and n , i.e., $\mu_i = \mu_i(T, p, \mathbf{n}\mathbf{y})$.

Of course, the dependence on n vanishes for large n and $\mu_i = \mu_i(T, p, \mathbf{y})$.

Mixture properties from the partial properties

So, in general (i.e., for small and large systems) we proved

$$S = \sum_{i=1}^r n_i s_i - \left(\frac{\partial Eu}{\partial T} \right)_{p,\mathbf{n}} \xrightarrow{n \text{ large}} S = \sum_{i=1}^r n_i s_i$$

$$V = \sum_{i=1}^r n_i v_i + \left(\frac{\partial Eu}{\partial p} \right)_{T,\mathbf{n}} \xrightarrow{n \text{ large}} V = \sum_{i=1}^r n_i v_i$$

$$\sum_{i=1}^r n_i \mu_{i,j} = - \left(\frac{\partial Eu}{\partial n_j} \right)_{T,p,\mathbf{n}'_j} \xrightarrow{n \text{ large}} \sum_{i=1}^r n_i \mu_{i,j} = 0 \quad \text{Duhem-Margules relation}$$

Moreover, recalling the definitions of Eu and partial properties

$$Eu = E - TS + pV - \boldsymbol{\mu} \cdot \mathbf{n} = F + pV - \boldsymbol{\mu} \cdot \mathbf{n} = G - \boldsymbol{\mu} \cdot \mathbf{n} = H - TS - \boldsymbol{\mu} \cdot \mathbf{n}$$

$$\mu_i = e_i - Ts_i + pv_i = f_i + pv_i = g_i = h_i - Ts_i$$

we also find the following relations, which justify calling partial properties that way:

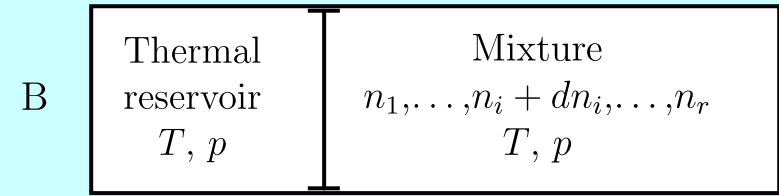
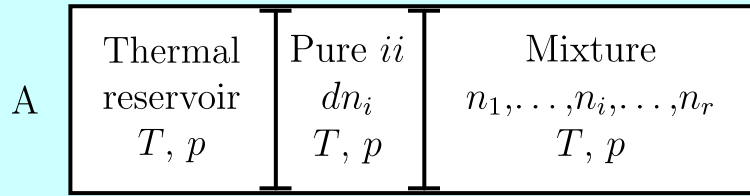
$$E = \sum_{i=1}^r n_i e_i + Eu - T \left(\frac{\partial Eu}{\partial T} \right)_{p,\mathbf{n}} - p \left(\frac{\partial Eu}{\partial p} \right)_{T,\mathbf{n}} \xrightarrow{n \text{ large}} E = \sum_{i=1}^r n_i e_i$$

$$F = \sum_{i=1}^r n_i f_i + Eu - p \left(\frac{\partial Eu}{\partial p} \right)_{T,\mathbf{n}} \xrightarrow{n \text{ large}} F = \sum_{i=1}^r n_i f_i$$

$$G = \sum_{i=1}^r n_i g_i + Eu = \sum_{i=1}^r n_i \mu_i + Eu \xrightarrow{n \text{ large}} G = \sum_{i=1}^r n_i g_i = \sum_{i=1}^r n_i \mu_i$$

$$H = \sum_{i=1}^r n_i h_i + Eu - T \left(\frac{\partial Eu}{\partial T} \right)_{p,\mathbf{n}} \xrightarrow{n \text{ large}} H = \sum_{i=1}^r n_i h_i$$

Partial properties from properties of isothermobaric mixing



Enthalpy of Tp -mixing*

$$\Delta h_i^{\text{mix}} = \frac{H(T, p, n_1, \dots, n_i + dn_i, \dots, n_r) - [H(T, p, n_1, \dots, n_i, \dots, n_r) + h_{ii}(T, p) dn_i]}{dn_i}$$

$$= \lim_{dn_i \rightarrow 0} \frac{H_B - H_A}{dn_i} = \left(\frac{\partial H}{\partial n_i} \right)_{T, p, n'_i} - h_{ii}(T, p) = h_i(T, p, n\mathbf{y}) - h_{ii}(T, p)$$

Similarly, we define the volume, energy, and entropy of Tp -mixing

$$\Delta v_i^{\text{mix}} = v_i(T, p, n\mathbf{y}) - v_{ii}(T, p) \quad \Delta e_i^{\text{mix}} = e_i(T, p, n\mathbf{y}) - e_{ii}(T, p) \quad \Delta s_i^{\text{mix}} = s_i(T, p, n\mathbf{y}) - s_{ii}(T, p)$$

They are all measurable and allow the measurement of partial properties, once the pure-substance properties of the mixture components are known. as a result, we can write

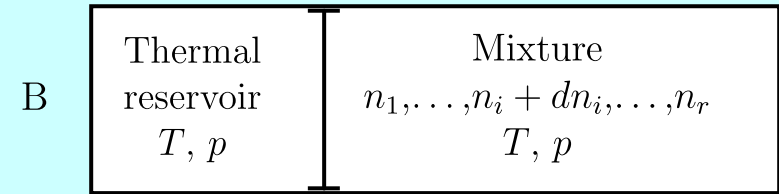
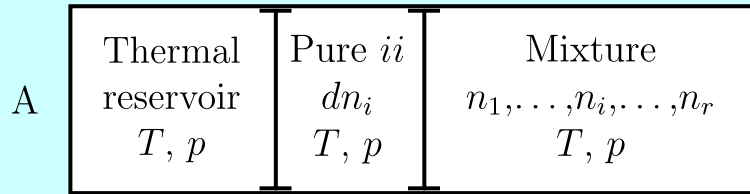
$$\mu_i = h_i - T s_i = h_{ii} + \Delta h_i^{\text{mix}} - T s_{ii} - T \Delta s_i^{\text{mix}} = \mu_{ii}(T, p) + \Delta h_i^{\text{mix}} - T \Delta s_i^{\text{mix}} = \mu_{ii}(T, p_{ii})$$

$$\mu_{ii}(T, p_{ii}) - \mu_{ii}(T, p) = \int_p^{p_{ii}} v_{ii}(T, p') dp' = \Delta h_i^{\text{mix}} - T \Delta s_i^{\text{mix}} = \begin{cases} RT \ln \frac{p_{ii}}{p} & \text{ideal gas} \\ -(p - p_{ii})v_{ii} & \text{ideal liquid or solid} \end{cases}$$

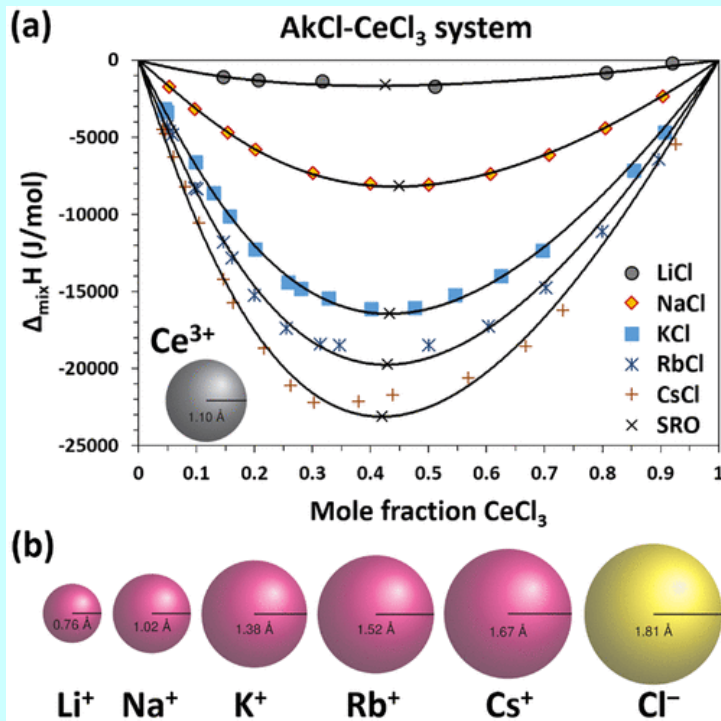
* Recall that the enthalpy is additive for systems in SES at the same pressure.

Experimental measurement of SES properties of mixtures:

Example: **enthalpies of isothermobaric mixing of molten salts**



$$\Delta h_i^{\text{mix}} = h_i(T, p, n\mathbf{y}) - h_{ii}(T, p)$$



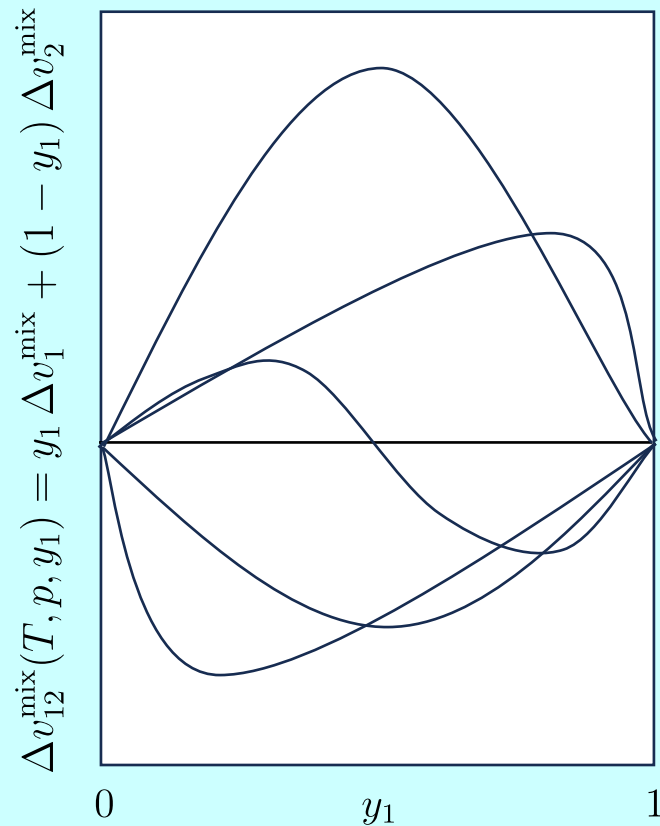
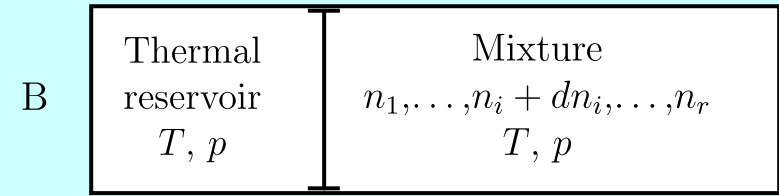
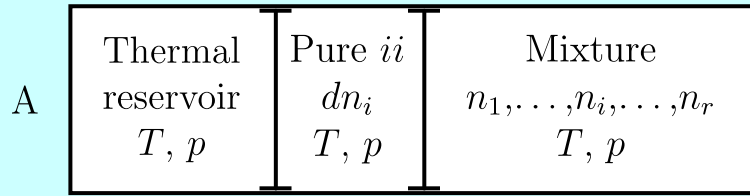
Last decade applications in molten salt systems:

- solvents for metals, particularly for extraction processes
- recycling and reprocessing of rare-earth elements used in electronics and magnets and nuclear fuels
- heat transfer media for solar-thermal systems and in molten salt reactors, which use salts as a coolant for solid fuel or as a solvent for a liquid fuel containing actinides

Fig.1 from: J. Schorne-Pinto, et al., [Correlational Approach to Predict the Enthalpy of Mixing for Chloride Melt Systems](#), *ACS Omega* 2022 7 (1), 362-371

Experimental measurement of SES properties of mixtures:

Example: **volumes of isothermobaric mixing of molten salts**



$$\Delta v_i^{\text{mix}} = v_i(T, p, n\mathbf{y}) - v_{ii}(T, p)$$

Reviews of experimental data:

Y.P. Handa, G.C. Benson, **Volume changes on mixing two liquids: A review of the experimental techniques and the literature data**, Fluid Phase Equilibria 3, 185 (1979).

R. Battino, **Volume changes on mixing for binary mixtures of liquids**, Chemical Reviews 71, 5 (1971).

Partial properties in terms of partial pressures and pure-substance properties

As discussed in Section 26.5 of G&B2005, it is noteworthy that the meaning of the term “partial” in the expression “partial pressure” is not the same as in the definition of “partial properties.” In fact, the partial pressure p_{ii} is not defined by a partial derivative with respect to amount n_i at constant T , p , and \mathbf{n}'_i . Nevertheless, partial properties can be expressed in terms of partial pressures and its derivatives as follows.

Recall that, by the definition of partial pressure, $\mu_{ii}(T, p_{ii}) = \mu_i(T, p, \mathbf{n}) = \mu_i(T, p, \mathbf{y})$ so that $p_{ii} = p_{ii}(T, p, \mathbf{y})$. Moreover, for the pure substance, $\mu_{ii}(T, p_{ii}) = g_{ii}(T, p_{ii})$ and $dg_{ii} = -s_{ii}(T, p_{ii}) dT + v_{ii}(T, p_{ii}) dp_{ii}$. We find

$$\begin{aligned} s_i(T, p, \mathbf{y}) &= -\left(\frac{\partial \mu_i}{\partial T}\right)_{p, \mathbf{n}} = -\left(\frac{\partial \mu_{ii}}{\partial T}\right)_{p_{ii}} - \left(\frac{\partial \mu_{ii}}{\partial p_{ii}}\right)_T \left(\frac{\partial p_{ii}}{\partial T}\right)_{p, \mathbf{n}} \\ &= s_{ii}(T, p_{ii}) - v_{ii}(T, p_{ii}) p_{ii, T}(T, p, \mathbf{y}) \quad \text{where we defined } p_{ii, T} = \left(\frac{\partial p_{ii}}{\partial T}\right)_{p, \mathbf{y}} \end{aligned}$$

$$\begin{aligned} v_i(T, p, \mathbf{y}) &= \left(\frac{\partial \mu_i}{\partial p}\right)_{T, \mathbf{n}} = \left(\frac{\partial \mu_{ii}}{\partial p_{ii}}\right)_T \left(\frac{\partial p_{ii}}{\partial p}\right)_{T, \mathbf{y}} \\ &= v_{ii}(T, p_{ii}) p_{ii, p}(T, p, \mathbf{y}) \quad \text{where we defined } p_{ii, p} = \left(\frac{\partial p_{ii}}{\partial p}\right)_{T, \mathbf{y}} \end{aligned}$$

$$h_i(T, p, \mathbf{y}) = \mu_i(T, p, \mathbf{n}) + T s_i(T, p, \mathbf{y}) = h_{ii}(T, p_{ii}) - T v_{ii}(T, p_{ii}) p_{ii, T}(T, p, \mathbf{y})$$

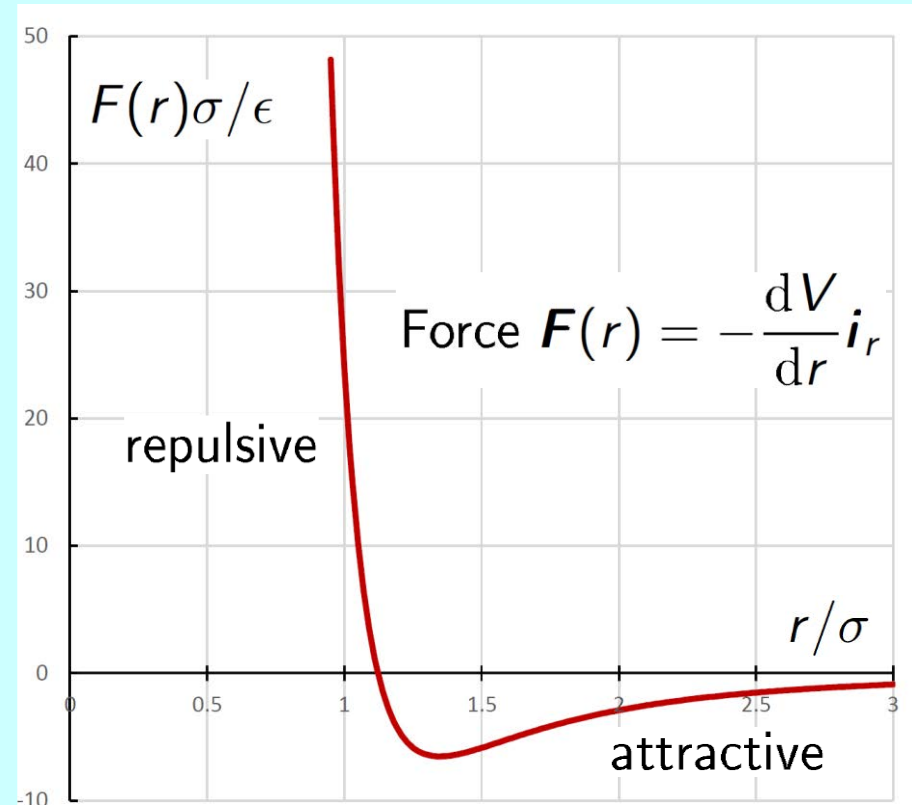
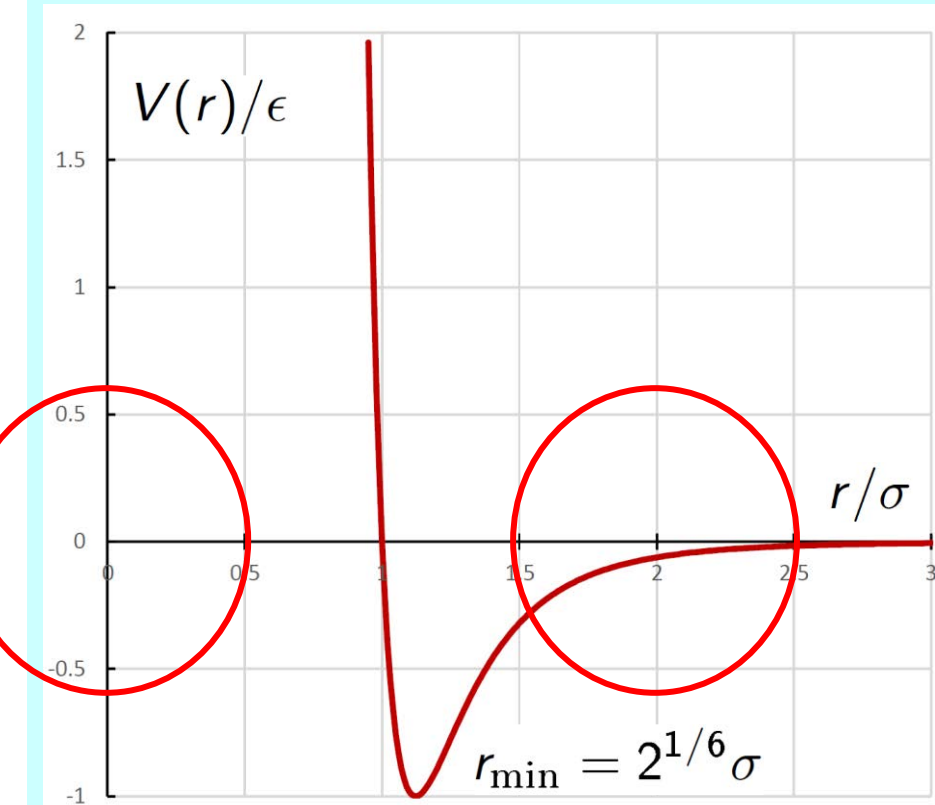
$$u_i(T, p, \mathbf{y}) = h_i(T, p, \mathbf{n}) - p v_i(T, p, \mathbf{y})$$

$$= u_{ii}(T, p_{ii}) + v_{ii}(T, p_{ii}) \left[p_{ii} - p_{ii, T}(T, p, \mathbf{y}) T - p_{ii, p}(T, p, \mathbf{y}) p \right]$$

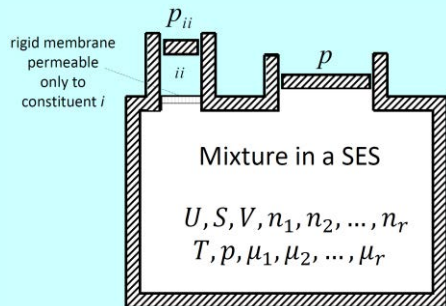
Lennard-Jones potential (model of intermolecular forces)

$$V(r) = 4\epsilon \left[\left(\frac{\sigma}{r} \right)^{12} - \left(\frac{\sigma}{r} \right)^6 \right]$$
$$= \epsilon \left[\left(\frac{r_{\min}}{r} \right)^{12} - 2 \left(\frac{r_{\min}}{r} \right)^6 \right]$$

$$F(r) = 24 \frac{\epsilon}{\sigma} \left(\frac{\sigma}{r} \right)^3 \left[2 \left(\frac{\sigma}{r} \right)^6 - 1 \right]$$
$$= 12 \frac{2^{2/3} \epsilon}{r_{\min}} \left(\frac{r_{\min}}{r} \right)^3 \left[\left(\frac{r_{\min}}{r} \right)^6 - 1 \right]$$



Ideal Gibbs-Dalton behavior



Ideal Gibbs-Dalton behavior is defined by

Assumption 1: $U = \sum_{i=1}^r n_i u_{ii}(T, p_{ii})$

Assumption 2: $S = \sum_{i=1}^r n_i s_{ii}(T, p_{ii})$

Assumption 3: $V = n_i v_{ii}(T, p_{ii}) \quad \forall i$

This derivation assumes the simple-system approximation.

Subtract from the Euler relation of the mixture, $U = TS - pV + \sum_{i=1}^r \mu_i n_i$, the specific Euler relations of its pure constituents, $u_{ii} = T s_{ii} - p_{ii} v_{ii} + \mu_{ii}$, evaluated at T and p_{ii} , and each multiplied by the amount n_i of the corresponding constituent in the mixture

$$\left(U - \sum_{i=1}^r n_i u_{ii}(T, p_{ii}) \right) = T \left(S - \sum_{i=1}^r n_i s_{ii}(T, p_{ii}) \right) - pV + \sum_{i=1}^r n_i p_{ii} v_{ii}(T, p_{ii}) + \sum_{i=1}^r (\mu_i - \mu_{ii}) n_i$$

The last summation is zero because at the specified conditions $\mu_i = \mu_i(T, p, \mathbf{n}) = \mu_{ii}(T, p_{ii}) = \mu_{ii}$. Now, solve for p (we may call this Dalton's theorem) to obtain a relation between the pressure of the mixture and the partial pressures of its components

$$p = \frac{1}{V} \sum_{i=1}^r n_i p_{ii} v_{ii}(T, p_{ii}) - \frac{1}{V} \left(U - \sum_{i=1}^r n_i u_{ii}(T, p_{ii}) \right) + \frac{T}{V} \left(S - \sum_{i=1}^r n_i s_{ii}(T, p_{ii}) \right)$$

Using the three assumptions that define ideal Gibbs-Dalton behavior, we obtain Dalton's law of partial pressures, $p = \sum_{i=1}^r p_{ii}$ (which clearly holds only in that very special limit).

Ideal Gibbs-Dalton behavior

Ideal Gibbs-Dalton behavior is defined by

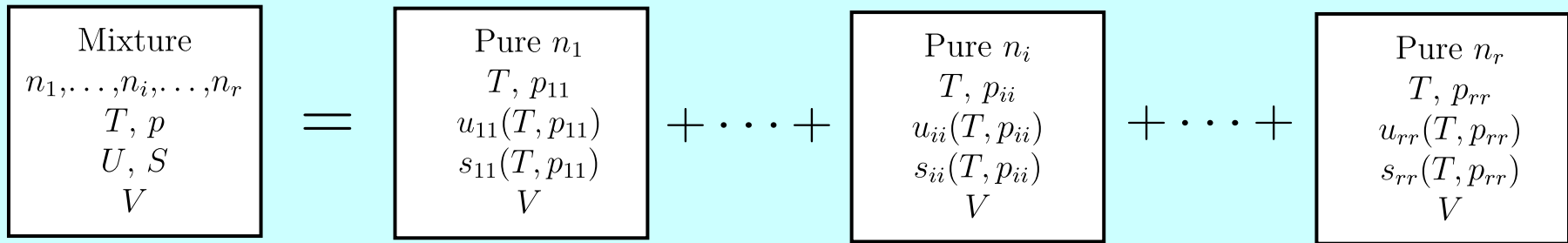
Assumption 1: $U = \sum_{i=1}^r n_i u_i(T, p, \mathbf{y}) = \sum_{i=1}^r n_i u_{ii}(T, p_{ii})$

Assumption 2: $S = \sum_{i=1}^r n_i s_i(T, p, \mathbf{y}) = \sum_{i=1}^r n_i s_{ii}(T, p_{ii})$

Assumption 3: $V = \sum_{i=1}^r n_i v_i(T, p, \mathbf{y}) = n_i v_{ii}(T, p_{ii}) \quad \forall i \quad (\text{no sum!})$

here the first equalities recall the relations in terms of partial properties.

The assumptions can be interpreted like this:



Ideal Gibbs-Dalton mixture of ideal gases

$$\forall i \text{ we have } v_{ii}(T, p_{ii}) = \frac{RT}{p_{ii}} \quad v_{ii}(T, p) = \frac{RT}{p} \quad V = n_i v_{ii}(T, p_{ii}) = n_i \frac{RT}{p_{ii}}$$

$$p_{ii} = n_i \frac{RT}{V} \quad p = \sum_i p_{ii} = \sum_i n_i \frac{RT}{V} = n \frac{RT}{V} \quad \frac{p_{ii}}{p} = \frac{n_i}{n} = y_i \quad \Rightarrow \quad p_{ii} = y_i p$$

$$\mu_i(T, p, \mathbf{y}) = \mu_{ii}(T, p_{ii}) = \mu_{ii}(T, p) + \int_p^{p_{ii}} \left(\frac{\partial \mu_{ii}}{\partial p} \right)_T dp' = \mu_{ii}(T, p) + \int_p^{p_{ii}} v_{ii}(T, p') dp'$$

$$= \mu_{ii}(T, p) + \int_p^{p_{ii}} \frac{RT}{p'} dp' = \mu_{ii}(T, p) + RT \ln \frac{p_{ii}}{p} = \mu_{ii}(T, p) + RT \ln y_i$$

Ideal Gibbs-Dalton mixtures of ideal gases

$$\forall i \text{ we have } v_{ii}(T, p_{ii}) = \frac{RT}{p_{ii}} \quad v_{ii}(T, p) = \frac{RT}{p} \quad V = n_i v_{ii}(T, p_{ii}) = n_i \frac{RT}{p_{ii}}$$

$$p_{ii} = n_i \frac{RT}{V} \quad p = \sum_i p_{ii} = \sum_i n_i \frac{RT}{V} = n \frac{RT}{V} \quad \frac{p_{ii}}{p} = \frac{n_i}{n} = y_i \Rightarrow p_{ii} = y_i p$$

$$\mu_i(T, p, \mathbf{y}) = \mu_{ii}(T, p_{ii}) = \mu_{ii}(T, p) + \int_p^{p_{ii}} \left(\frac{\partial \mu_{ii}}{\partial p} \right)_T dp' = \mu_{ii}(T, p) + \int_p^{p_{ii}} v_{ii}(T, p') dp'$$

$$= \mu_{ii}(T, p) + \int_p^{p_{ii}} \frac{RT}{p'} dp' = \mu_{ii}(T, p) + RT \ln \frac{p_{ii}}{p} = \mu_{ii}(T, p) + RT \ln y_i$$

$$s_i(T, p, \mathbf{y}) = - \left(\frac{\partial \mu_i}{\partial T} \right)_{p, \mathbf{n}} = s_{ii}(T, p) - R \ln y_i = s_{ii}(T, p_{ii}) \quad v_i(T, p, \mathbf{y}) = \left(\frac{\partial \mu_i}{\partial p} \right)_{T, \mathbf{n}} = v_{ii}(T, p) = \frac{RT}{p}$$

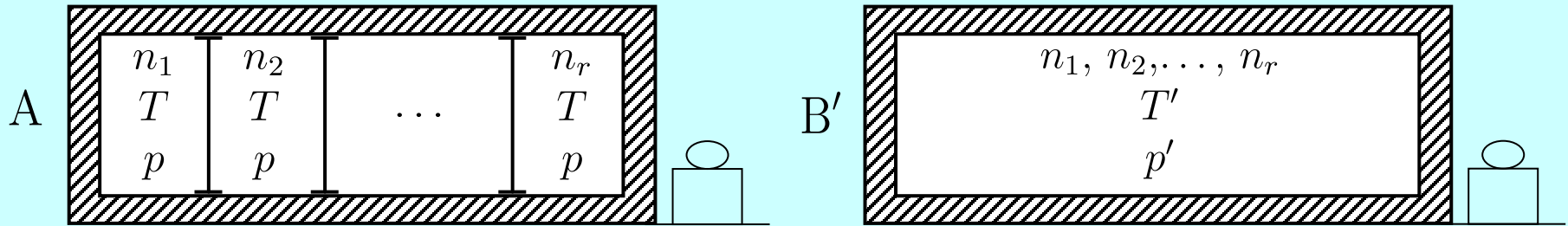
$$h_i(T, p, \mathbf{y}) = \left(\frac{\partial(\mu_i/T)}{\partial(1/T)} \right)_{p, \mathbf{n}} = h_{ii}(T) \quad u_i(T, p, \mathbf{y}) = T s_i - p v_i + \mu_i = u_{ii}(T)$$

Note also that $V = \sum_{i=1}^r V_i' = \sum_{i=1}^r n_i v_{ii}(T, p)$ (Amagat law of additive volumes)

where $V_i' = n_i v_{ii}(T, p)$ is called proper volume of i

Mixture $n_1, \dots, n_i, \dots, n_r$ T, p U, S V	=	Pure n_1 T, p $u_{11}(T)$ $s_{11}(T, p)$ $V_1' = \frac{n_1 RT}{p}$	Pure n_2 T, p $u_{22}(T)$ $s_{22}(T, p)$ $V_2' = \frac{n_2 RT}{p}$. . .	Pure n_r T, p $u_{rr}(T)$ $s_{rr}(T, p)$ $V_r' = \frac{n_r RT}{p}$
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Entropy of spontaneous mixing



Remove partitions allowing spontaneous mixing. Using energy, volume, and entropy additivity for A, and ideal G-D-mixture model for B',

$$U_A = \sum_i n_i u_{ii}(T) \quad V_A = \sum_i n_i v_{ii}(T, p) = \frac{nRT}{p} \quad S_A = \sum_i n_i s_{ii}(T, p)$$

$$U_{B'} = \sum_i n_i u_{ii}(T') \quad V_{B'} = \sum_i n_i v_{ii}(T', p') = \frac{nRT'}{p'} \quad S_{B'} = \sum_i n_i s_{ii}(T', p'_{ii})$$

Energy balance for the isolated system, $U_{B'} - U_A = 0$, recalling $du_{ii} = c_{v,ii}(T) dT$,

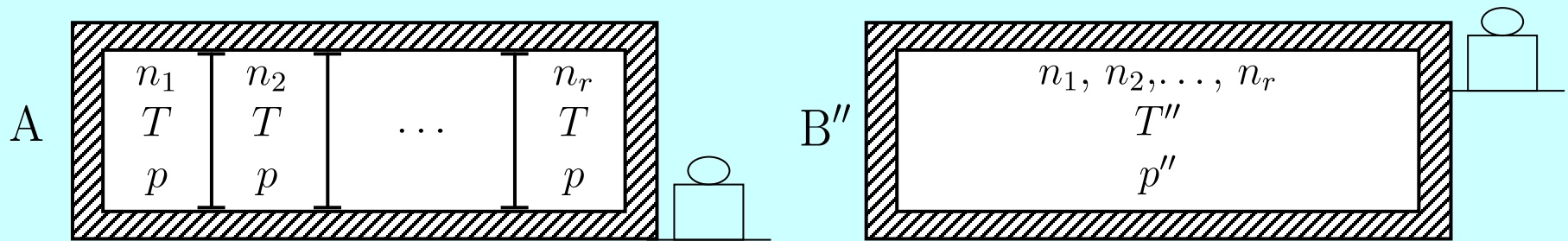
$$U_{B'} - U_A = \sum_i n_i [u_{ii}(T') - u_{ii}(T)] = \sum_i n_i \int_T^{T'} c_{v,ii}(\theta) d\theta = 0$$

Since $c_{v,ii}(T) > 0$ for any T , the integral can only be zero if $T' = T$. Therefore, the volume balance $V_{B'} = V_A$ yields $p' = p$.

Entropy balance for the isolated system, $S_{B'} - S_A = S_{\text{irr}}$, recalling $ds_{ii} = c_{p,ii}(T) dT/T - R dp/p$, so that $s_{ii}(T', p'_{ii}) = s_{ii}(T', p) - R \ln y_i$, yields (for $T' = T$ and $p' = p$)

$$S_{\text{irr}} = S_{B'} - S_A = \sum_i n_i [s_{ii}(T', p'_{ii}) - s_{ii}(T, p)] = \sum_i n_i \Delta s_i^{\text{mix}} = \sum_i n_i [-R \ln y_i] = -nR \sum_i y_i \ln y_i \geq 0$$

Extracting the adiabatic availability of mixing



Do the mixing with a reversible weight process. Using energy, volume, and entropy additivity for A, and ideal G-D-mixture model for B'',

$$U_A = \sum_i n_i u_{ii}(T) \quad V_A = \sum_i n_i v_{ii}(T, p) = \frac{nRT}{p} \quad S_A = \sum_i n_i s_{ii}(T, p)$$

$$U_{B''} = \sum_i n_i u_{ii}(T'') \quad V_{B''} = \sum_i n_i v_{ii}(T'', p'') = \frac{nRT''}{p''} \quad S_{B''} = \sum_i n_i s_{ii}(T'', p''_{ii})$$

The volume balance $V_{B''} = V_A$ imposes $p''/T'' = p/T$. Thus, recalling $p''_{ii} = y_i p''$, assuming constant specific heats, defining $c_{v,mix} = \sum_i y_i c_{v,ii}$, and using

$$s_{ii}\left(T'', p''_{ii} = y_i \frac{T''}{T} p\right) - s_{ii}(T, p) = c_{p,ii} \ln \frac{T''}{T} - R \ln \left(y_i \frac{T''}{T}\right) = c_{v,ii} \ln \frac{T''}{T} - R \ln y_i$$

the entropy balance for the reversible weight process, $S_{B''} - S_A = 0$, becomes

$$0 = S_{B''} - S_A = \sum_i n_i [s_{ii}(T'', p''_{ii}) - s_{ii}(T, p)] = \sum_i n_i [c_{v,ii} \ln \frac{T''}{T} - R \ln y_i] = n [c_{v,mix} \ln \frac{T''}{T} - R \sum_i y_i \ln y_i]$$

and yields $T'' = T \exp\left(\frac{R}{c_{v,mix}} \sum_i y_i \ln y_i\right)$ (clearly $T'' < T$). Therefore, the energy balance for the weight process, $U_{B''} - U_A = -W_{rev}^{\rightarrow}$, yields

$$W_{rev}^{\rightarrow} = U_A - U_{B''} = \sum_i n_i [u_{ii}(T'') - u_{ii}(T)] = n c_{v,mix} (T - T'') = n c_{v,mix} T \left[1 - \exp\left(\frac{R}{c_{v,mix}} \sum_i y_i \ln y_i\right)\right]$$

Extracting the adiabatic availability of mixing

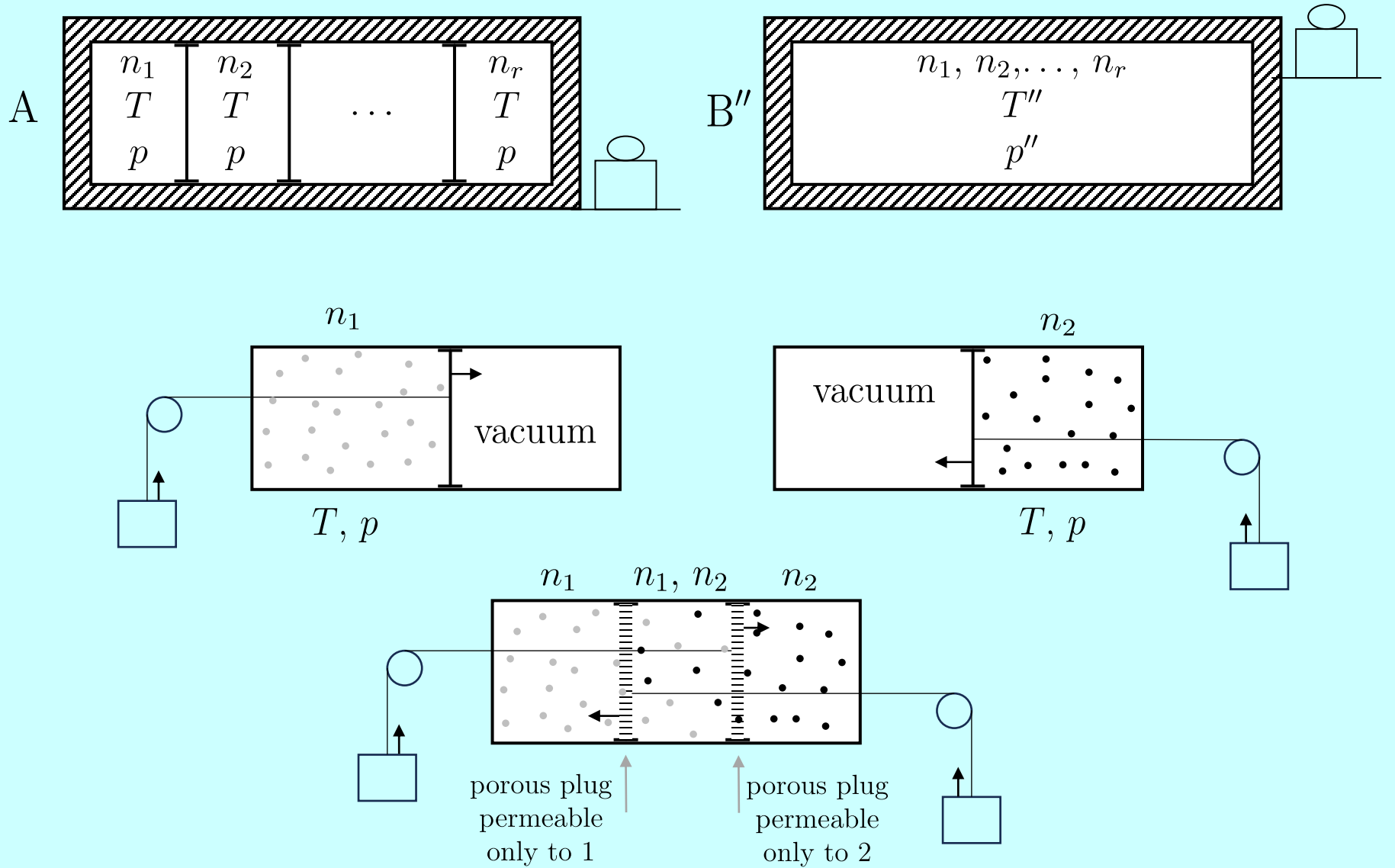


Image Credits

Slide 6:

Enthalpy of mixing for the alkali series with cerium trichloride and ionic radii of alkali elements and chlorine © American Chemical Society. All rights reserved. This content is excluded from our Creative Commons license. For more information, see <https://ocw.mit.edu/help/faq-fair-use>.

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