Lecture # 5

Chemical Thermodynamics 1

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- Mass conservation in chemical reactions
- Energy conservation in chemical reactions
- Fuels and chemical energy carriers ……
- Combustion and Flame temperature.

Stoichiometry (element conservation) & Mass Conservation

Complete oxidation (burning) or reduction of "chemical energy carriers":

oxidation : $2H_2+O_2 \Rightarrow 2H_2O(\pm energy)$ $reduction: 2H₂O \Rightarrow 2H₂+O₂$ (*±energy*) $CH_4 + 2(O_2 + 3.76N_2) \Rightarrow CO_2 + 2H_2O + 7.52N_2$

Stoichiometric generic reaction: $\sum v_i' \chi_i \Rightarrow \sum v_i'' \chi_i$ *react prod*

mass or elemental balance: $\sum v_i' v_{ij}^* = \sum v_i' v_{ij}^*$, or $\sum v_i v_{ij}^* = 0$ for $j = 1, J$ v_i ['] and v_i ["] are the stoichiometric coefficient satisfying conservation of element. *react prod react*

 v_{ij}^* is the number of *j* atom in *i* molecule.

The molar stoichiometric air-fuel ratio:

$$
\widehat{AF}_{ST} = \left(\frac{n_{air}}{n_{fuel}}\right)_{ST} = \left(\frac{n_{oxygen} + n_{nitrogen}}{n_{fuel}}\right)_{ST} = \frac{v_{oxygen}^{'} + v_{nitrogen}^{'}}{v_{fuel}^{'}}
$$
 (a mole has N_a=6.022 10²³ molecules) for methane-air: $\widehat{AF}_{ST} = 2(1+3.76) = 9.52$

The mass-based stoichiometric air-fuel ratio $AF_{ST} = \frac{m_{air}}{m_{air}}$

$$
AF_{ST} = \left(\frac{m_{air}}{m_{fuel}}\right)_{ST} = \frac{v_{oxygen}^{'}M_{oxygen} + v_{nitrogen}^{'}M_{oxygen}}{v_{fuel}^{'}M_{fuel}}
$$

For methane-air:
$$
AF_{ST} = 2(32+3.76 \times 28)/(12+4) = 17.16
$$

For non stoichiometric reactions/combustion: $\widehat{AF} =$

$$
\widehat{AF} = \left(\frac{n_{air}}{n_{fuel}}\right) = \left(\frac{n_{oxygen} + n_{nitrogen}}{n_{fuel}}\right)
$$

The ratio between the actual and stoichiometric is:the excess air ratio is:

$$
\lambda = \frac{AF}{AF_{ST}}
$$
, and the equivalence ratio: $\phi = \frac{1}{\lambda}$

(Fuel) Lean and rich burn

Lean Burning, ϕ < 1 (in many power plants, burners and diesel engines). Likely to lead to complete combustion, low NOx formation (becasue of low T):

 $CH_4 + 2.4(O_2 + 3.76N_2) \Rightarrow CO_2 + 2H_2O + 0.4O_2 + 9.024N_2$

Rich Burning, $\phi > 1$, used in partial oxidation, fuel reforming and production of syngas, hydrogen, etc,

Example: partial oxidation (exothermic) for coal gasification/biochar: $C + \frac{1}{2}O_2 \Rightarrow CO$,

 $CH_4 + \frac{1}{2}O_2 \Rightarrow CO + 2H_2$ and methane partial oxidation

Not all reactions involve fuel oxygen!

Rerforming (endothermic) can also be steam gasification $C+H_2O \Rightarrow CO+H_2$ and methane reforming $CH_4 + H_2O \Rightarrow CO + 3H_2$ More hydrogen can be produced by the "water-gas shift": $CO+H_2O \Rightarrow CO_2+H_2$

Thermodynamic Properties of Fuel Combustion at 25 C and 1 atm Pressure

 \blacksquare

FHV=LHV (water in the products in the vapor phase)

 Δg is the Gibbs free energy of reaction (maximum work under isothermal reaction conditions). Last column: the heating value/carbon = FHV*molecular weight of fuel/molecular weight of carbon.

Fossil/Organic/Hydrocarbon Fuels

COAL, OIL, NATURAL GAS. OIL SHALE, TAR SANDS, PEAT. "BIOMASS".. Young, "renewable".

- Formed due to the fossilization of *organic* matter, underground (although evidence of earth mantel inorganic (abiogenic) methane is rising).
- All formed of carbon and hydrogen, some with little oxygen, plus sulfur, mercury and other minerals, and non combustibles.
- Most require some form of processing: sulfur removal, grinding and washing, oil refining, gas desulfurization.

Energy Balance in Chemical Reactions

$$
\frac{dE}{dt} = \dot{Q} - \dot{W} + \left(\sum_{react} \dot{m}_i \left(h_i + V_i^2 + g_v z_i\right) - \sum_{prod} \dot{m}_i \left(h_i + V_i^2 + g_v z_i\right)\right)
$$
\n
$$
h_i = h_{i, thermal} + h_{i,chemical} = \int_{T^o}^{T} c_{p,i} dT + h_{i,chemical}^o
$$
\n
$$
\text{state 1}
$$

Steady, constant pressure and temperature, one mole of fuel:

$$
Q = \sum_{\text{prod}} n_i \hat{h}_i - \sum_{\text{react}} n_i \hat{h}_i \quad (\text{ = heating value of the fuel})
$$

• heat transfer out of the reaction, at constant p and T is *the enthalpy of reaction*.

$$
H_2 + \frac{1}{2}(O_2 + 3.76N_2) \to H_2O + \frac{3.76}{2}N_2 \quad \left\| + \Delta \hat{h}_{H2O}^o \right\|
$$

$$
\Delta \hat{h}^o_{\text{fuel}} = \sum_{\text{prod}} v_i^{\dagger} \hat{h}^o_i - \sum_{\text{react}} v_i^{\dagger} \hat{h}^o_i, \quad v_i \text{ is the soichiometric coefficient}
$$

⁷ © by Ahmed F. Ghoniem

• Need to define a reference for the enthalpies.

Reference Enthalpy, Enthalpy of Formation *N N* $H = \sum m_i h_i(T, p_i) = \sum n_i \hat{h}_i(T, p_i)$ *i*=1 *i*=1 $h_i = h_{f,i}^o + \int_{T^o}^T c_{p,i}(T) dT$, and $\hat{h}_i = \hat{h}_f^o$ *T* $c_{p,i}(T) dT$, and $\hat{h}_i = \hat{h}_{f,i}^o + \int$ *T* $\hat{c}_{p,i}(T) dT$ T^o ^{*p*}, *i* T^o *f* T^o $\hat{h}_{f}^{o} \equiv \Delta \hat{h}_{f}^{o}$

Reference Entropy

Enthalpy of Formation

$$
Formation Reaction: \qquad \sum_{i} V_{i} \chi_{i} \Rightarrow \chi_{comp}
$$

$$
\Delta \hat{h}_R^o = \hat{h}_{comp}^o - \sum_i v_i \hat{h}_i^o = \hat{h}_{comp}^o
$$
 for formation reaction ...
Enthalpy of reaction of stable molecules, in their phase at STP,

is taken to be zero:

$$
O_{2(g)},\,N_{2(g)},\,H_{2(g)},\,C_{(s,\,graphite)}
$$

Formation reaction of methane: $C_{(s)} + 2H_{2(g)} \Rightarrow CH_{4(g)}$

Energy of formation accounts for the net energy required to form or break bonds in a complex molecule. $\frac{C_1}{C_2}$ H methane $H - C - H$ methane

Types of bonds: single, double, … depending on the number of shared electrons. C has four bonds. H H H

A saturated HC, like methane and methanol, use the four C bonds to attach another atom (H or C or a functional group (OH)) H H H

Single C –C bond 248 MJ/kmol Double C=C bond 615 MJ/kmol Triple ….. 812 MJ/kmol

Double O=O 498 MJ/kmol

…

O-OH 498 MJ/kmol $H-O2$ 196 MJ/kmol 10

Enthalpy of Reaction, Steady, constant p, zero work, etc.

Arbitrary mixture

$$
Q = H_{out}(T_{out}) - H_{in}(T_{in}) = \sum_{prod} n_i \hat{h}_i - \sum_{react} n_i \hat{h}_i
$$

stoichiometric at STP (same T^o) $h \rightarrow$) *^h*

$$
\Delta H_{R}^{o} = \sum_{prod} v_{i}^{"} \hat{h}_{i}^{o} - \sum_{react} v_{i}^{"} \hat{h}_{i}^{o}
$$

stoichiometric at arbitrary T

$$
\Delta H_R(T) = \sum_{prod} v_i \hat{h}_i(T) - \sum_{react} v_i \hat{h}_i(T) = \sum_{species} v_i \hat{h}_i(T)
$$

$$
v_i = v_i - v_i
$$

T

Examples:

$$
CO + \frac{1}{2}O_2 \Rightarrow CO_2
$$

$$
Q^o = \hat{h}_{CO2}^o - \left(\hat{h}_{CO}^o + \frac{1}{2}\hat{h}_{O2}^o\right) = -393 - (-110.6 + 0) = -282.5 \text{ kJ/gmol of CO}
$$

$$
C_nH_m + \left(n + \frac{m}{4}\right)(O_2 + 3.76N_2) \Rightarrow nCO_2 + \frac{m}{2}H_2O + \left(n + \frac{m}{4}\right)3.76N_2
$$

$$
\Delta \hat{H}_{R,C_nH_m}^o = n\hat{h}_{CO_2}^o + \frac{m}{2}\hat{h}_{H_2O}^o - \hat{h}_{C_nH_m}^o = \Delta \hat{h}_{R,C_nH_m}^o
$$

For methane-air combustion, the "standard" enthalpy of reaction is:

$$
\Delta \hat{h}^{\circ}_{CH_4} = -393.8 + 2(-242) - (-74.9) = -802.9 \text{ MJ/kgmol of methane}
$$

FHV=LHV (water in the products in the vapor phase)

Dg is the Gibbs free energy of reaction (maximum work under isothermal reaction conditions). Last column: the heating value/carbon = FHV*molecular weight of fuel/molecular weight of carbon.

The Heating Value of a fuel is |enthalpy of reaction| per mole, The table shows the LHV (water in vapor form). HHV is obtained when water comes out in liquid form.

adiabatic combustion:

$$
\hat{h}_{CH4}^{27C} + \alpha \left(\hat{h}_{O2}^{205C} + 3.76 \hat{h}_{N2}^{205C} \right) = \hat{h}_{CO2}^{950C} + 2 \hat{h}_{H2O}^{950C} + (\alpha - 2) \hat{h}_{O2}^{950C} + 3.76 \alpha \hat{h}_{N2}^{950C}
$$

solve using enthalpy expressions: $\alpha = 7.428$ (for stoichiometric: $\alpha = 2$)

Hydrocarbon Combustion in Air

$$
C_nH_m + \left(n + \frac{m}{4}\right)(O_2 + 3.76N_2) \to nCO_2 + \frac{m}{2}H_2O + 3.76\left(n + \frac{m}{4}\right)N_2
$$

- Hydrocarbons store energy in their chemical bonds. Highest energy storage per unit mass or unit volume (in liquid/solid forms).
- Chemical Energy is converted into thermal energy during combustion, or to other forms of chemical energy during refining and reforming (processes that may require energy).
- In complete, *stoichiometric* combustion of hydrocarbons, the products are water and carbon dioxide.

The table shows the LHV (water in vapor form)*,* in MJ/kg fuel.

Commercial Fuels

Biomass Fuels

OAL

(fossilized vegetations) lignite, subbituminous, bituminous, anthracite.

- Coal is carbon + hydrogen $(CH_m, m \le 1)$ + sulfur (up to 10% by weight) + nitrogen + $oxygen + ash$ (non combustibles).
- Heating value per unit mass increases from lignite to anthracite, as the carbon ratio grow (and moisture, volatile matter including H_2 ratio, and sulfur decrease).
- Some sulfur can be washed away before combustion, but mostly is scrubbed from combustion products using limestone.
- In gasification, rich burning in oxygen and water forms syngas $(CO+H₂)$, desulfurization before combustion or gas separation.

OIL

(or petroleum, liquid rock, fossilized marine life. algae)

- Made up of many organic compounds + hydrogen + nitrogen + sulfur. Sweet and sour refer to the amount of sulfur. CH_m, $1 \le m \le 2$.
- "Light oil" is generally composed of three hydrocarbon families:
	- Saturated hydrocarbons: normal alkanes (paraffins), C_nH_{2n+2} , with gas, n = 1-4, liquid, $n = 5-15$, and solids, $n > 15$.
	- Unsaturated hydrocarbons, and aromatics like benzene, C_6H_6 , toluene, C_7H_8 and nephthalene, $C_{10}H_8$.
	- Resin and asphaltenes, heavier hydrocarbons rich in nitrogen, oxygen, sulfur and vanadium.
- Refining: distillation (separation of lighter components), catalytic cracking (heating) and reforming (with steam or hydrogen). Products are typically refinery gas, LPG, gasoline (mostly octane C_8H_{18}), aviation fuels (JPx), diesels, heating and lube oils ...

A Large Demand for Hydrogen is due to the **Declining Quality of Available Crude Oil** ORNL DWG 2001-107R2

Image courtesy of Idaho National Laboratory, DOE.

Non-Conventional "Heavy" Oil (all require intensive processing)

Oil Shale:

impermeable hard rock containing (organic, non petroleum) *kerogen* (pre-oil), which pyrolyzes into oil + (organic, petroleum) *bitumen* that liquefies with heating.

Tar and Tar Sands:

a mixture of sand and *bitumen* (coal-like), the bitumen is extracted by heating and steam, and it can be refined into oil components.

After slowing down in 2016, U.S. shale oil is expected to ramp up again in 2017, continuing a decade-long surge. Constructed by Lucas Davis (UC Berkeley) using EIA data.

Courtesy of [Lindsey G](https://www.flickr.com/people/61687036@N08) on [Wikimedia](https://commons.wikimedia.org/wiki/File:Williston_North_Dakota_Oil_Field_Oil_Rig_(5894614162).jpg). License: CC BY.
Figure courtesy of Lucas Davis, UC Berkeley. Used with permission.

U.S. oil production in 2015 reached its highest level in decades, driven large increases in production from shale oil. …. Ford, Permian, and Bakken, but other areas have grown rapidly as well, and shale oil now represents almost half of all U.S. production.

NATURAL GAS

- Mostly methane, CH_4 , ethane C_2H_6 , some propane, C_3H_8 , and little butane, C_4H_8 , with small fractions of higher hydrocarbons, may contain sulfur, oxygen, $CO₂$ at small quantities.
- Requires least processing.
- Biogenic Gas: near surface, difficult to exploit.
- **Methane hydrides/hydrates**, found in deep oceans, and permafrost, encapsulated in water (estimated to exceed 2 orders of magnitude of proven gas reserves) in ice like structures.
- Shale gas, like shale oil.
- Abiogenic gas, deep underground, non organic

Adiabatic Flame Temperature

 $CH_4+2(O_2+3.76N_2) \Rightarrow CO_2+2H_2O+7.52N_2$ starting with $T = 298$ K $\sum v_i \hat{h}_i(298) = \hat{h}_{\text{methane}}^o = -74,831 \text{ kJ/kgmole}$ *react* $\hat{h}_{CO_2}(T_p) + 2\hat{h}_{H_2O}(T_p) + 7.52\hat{h}_{N_2}(T_p) = \sum^3 n_i \hat{h}_i^o + \sum^3 n_i \int_{-\infty}^{T_p}$ $\hat{L}_{CO_2}(T_p) + 2\hat{h}_{H_2O}(T_p) + 7.52\hat{h}_{H_2O}(T_p)$ $N_2(T_p) = \sum_{i=1}^{n} n_i \hat{h}_i^o + \sum_{i=1}^{n} n_i \int_{T_o}^{T_p} \hat{c}_{p,i} dT$ $\sum_{i=1}^{\infty}$ $\sum_{i=1}^{\infty}$ $\sum_{j=1}^{\infty}$

By iteration: $T = 2340$ K.

The adiabatic flame temperature is highest at conditions slightly richer than stoichiometric (because of dissociation). Most fuels peak around 2300-2400 K, hydrogen's and CO are higher, and acetylene is the highest. *Lean* and *rich* burn, or lower and higher equivalence ratios, lead to lower flame temperature, with the latter containing **Exerced Containing** Excluded from our Creative Commons license. For more fuel fragments. Oxy-combustion is much higher. The state of the st

Combustion in a Closed Volume

$$
Q - W = \Delta U = U_p - U_r
$$

= $H_p - H_r - ((p\forall)_p - (p\forall)_r)$
= $\sum_{prod} n_i \hat{h}_i(T_p) - \sum_{react} n_i \hat{h}_i(T_r) - (n_p \Re T_p - n_r \Re T_r)$

"Standard" Internal Energy of Reaction

$$
\Delta \hat{U}_R^o = \sum_{prod} v_i \hat{h}_i(T^0) - \sum_{react} v_i \hat{h}_i(T^0) - (v_p - v_r) \Re T^0
$$

= $\Delta \hat{H}_R^o - (v_p - v_r) \Re T^0$
 $v_p = \sum v'', \quad v_r = \sum v'$

 The complete combustion of various hydrocarbons in a **perfectly insulated constant-volum e com bustion chamber,** stoichiometric mixture with dry air starting at 298 C and 1 atm. from Gyftopoulos and Beretta

Efficiency

Combustion:
$$
(\eta_{comb})_l = \frac{\sum_{prod} n_i \hat{h}_i - \sum_{react} n_i \hat{h}_i}{- \hat{h}_{R,f}} = \frac{Q_H}{HV_{field}}
$$
 < 1 , (incomplete combustion; heat losses)
For engines and FC (chemical engines: $\eta_{fuel-utiliz} = \frac{\dot{W}_{net}}{\dot{m}_{fuel}HV_{field}}$
OR: $\eta_{fuel-utiliz} = \frac{W_{net}}{W_{max}} \frac{W_{max}}{Q_H} \frac{Q_H}{HV_{field}} = \eta_H . \eta_{car} . \eta_{comb}$
For fuel production: $(\eta_{refom})_l = \frac{\text{Energies Out}}{\text{Energies In}} = \frac{\text{Chemical Energy Out}}{\text{Chemical Energy In}} = \frac{(\dot{n}_f \Delta \hat{h}_f)_{out}}{\sum_{in} (\dot{n}_f \Delta \hat{h}_f)}$

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