Lecture #8 Electrochemical Thermodynamics 1

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- Electrochemical reactions
- Electrodes and electrolytes
- Fuel cell components
- Work generated by a fuel cell
- Voltage and Ideal Efficiency

Heat engine (heat to work) efficiency

 Ideal thermo-mechanical efficiency using practically achievable/manageable temperatures is 70-85%!

Engines running on adiabatic combustion

Keeping the reaction isothermal and in equilibrium with the environment produces maximum work

 $Q-W = H_{out} - H_{in} = \Delta H_R$ *Q* T^* $=S_{\omega t} - S_{\text{in}} = \Delta S_R$ $Q = T \Delta S_R$ heat added $-W = (H - TS)_{out} - (H - TS)_{in}$ $=\Delta H_R - T \Delta S_R$ $W = -\Delta G_R$ work produced.

The isothermal reaction produces work = Gibbs free energy of reaction, and rejects heat $= T$. entropy of reaction

 for typical exothermic reactions, both ΔH_R and $\Delta G_R < 0$

and heat is mostly rejected

(but can also be added) depending on T

How can we perform such an isothermal reaction with work transfer?

The overall Reaction: $H_2 + \frac{1}{2}O_2 \Rightarrow H_2O$ 2

 *c*an be performed in a Redox Pair (reduction-oxidation), or two electrochemical "half reactions", across an electronically non-conducting material, leading to the formation of charged species; $Hydrogen$ Oxidation: $H_2 \Rightarrow 2H^+ + 2e^-$ Hydrogen loses e- \overline{a}

Hydrogen Reduction: $\frac{1}{2}O_2 + 2e^+ + 2H^+ \Rightarrow H_2O$ Reactants gain e 2

H⁺ ions diffuse through the electrolyte (acidic, +ve ion (proton) transport medium (PEM*FC*)

e- moves through an external resistance

 A useful note: the general definition of oxidation and reductions: Oxidation is Loss of electron (loss of -ve charge or becoming positive) Reduction is Gain of electron (gain of -ve charge of becoming negative) $Hydrogen$ Oxidation: $H_2 \Rightarrow 2H^+ + 2e^-$ Hydrogen loses e-*Hydrogen* Reduction: $\frac{1}{2}O_2 + 2e^+ + 2H^+ \Rightarrow H_2O$ Reactants gain e 2 Reactants gain e-

 Galvanic or voltaic cell. At finite current, $\Delta V < \Delta \mathcal{E}$. In galvanic cells the anode is the -ve electrode and the cathode is the +ve electrode.

Another redox pair uses an alkaline electrolyte (transports -ve ions):

Hydrogen Oxidation, Anode: $H_2 +$ $O²$ ions move through the electrive from the cathode to the anode Overall Reaction: $H_2 + \frac{1}{2}O_2 \Rightarrow H_2O$ Oxygen Reduction, Cathode: $\frac{1}{2}O_2 + 2e^- \rightarrow O^2$ 1 $O^2 \rightarrow H_2O + 2e^-$ 2

CO Electrochemical Oxidation

Overall Reaction: $CO + \frac{1}{2}O_2 \Rightarrow CO_2$ The Redox Pair (two half reaction) Oxidation, Anode: $CO + O^2 \rightarrow CO_2 + 2e^-$ Can combine H_2 and CO in a single cell 1 Reduction, Cathode: $\frac{1}{2}O_2 + 2e^- \rightarrow O^2$

Open circuit Work:

$$
\left(-\Delta G_R(T^*, p^*)\right) = \sum_{react} v_i' \left(\hat{h}_i(T^*) - T^* \hat{s}_i(T^*, p^*)\right) - \sum_{prod} v_i'' \left(\hat{h}_i(T^*) - T^* \hat{s}_i(T^*, p^*)\right)
$$

$$
= \left(-\Delta G_R^o(T^*)\right) - \sigma \mathfrak{R} T^* \ln\left(\frac{p^*}{p^o}\right) - \mathfrak{R} T^* \ln\left(\frac{\prod_{prod} X_i^{v_i}}{\prod_{real} X_i^{v_i}}\right)
$$

$$
\Delta G_R^o(T^*) = \sum_{react} v_i' \left(\hat{h}_i(T^*) - T\hat{s}_i^o(T^*)\right) - \sum_{prod} v_i'' \left(\hat{h}_i(T^*) - T\hat{s}_i^o(T^*)\right)
$$

Important remarks:

- 1. Reactants are introduced separately.
- 2. Products mix with one of the reactant stream
- 3. Or products leave separately through the electrolyte.

Equilibrium or Open-circuit Efficiency:

$$
\eta_{OC} = \frac{W_{\text{max}}}{\Delta H_{R,H_2O}^*} = \frac{\Delta G_{R,H_2O}^*}{\Delta H_{R,H_2O}^*}
$$

For separate streams for hydrogen, oxygen and water: All at 1 atm

$$
\Delta G_R^o(T) = (\hat{h}(T) - T\hat{s}^o(T))_{H_2O} - \left[(\hat{h}(T) - T\hat{s}^o(T))_{H_2} + \frac{1}{2} (\hat{h}(T) - T\hat{s}^o(T))_{O_2} \right]
$$

$$
\hat{s}^o(T) = \hat{s}(T, p = 1 \text{ atm})
$$

$$
\eta_{OC} = \frac{\Delta G_{R,H_2O}^*}{HHV_{H_2O}}
$$

 ω T = 300 K: water leaving as liquid: $\eta_{OC} = 237/286$)=83% (water leaving as vapor: $\eta_{\text{OC}} = 228/242 = 94\%$)

 ω T = 500 K: water leaving as vapor: $\eta_{OC} = 219/242 = 76.5\%$ $\omega_{\text{C}} = 1000 \text{ K}$: water leaving as vapor: $\eta_{\text{OC}} = 193 / 245 = 67.3\%$ © Source unknown . All rights reserved. This content is excluded from our Creative Commons license. For more information, see https://ocw.mit.edu/fairuse

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- a simple Carnot engine. • Reversible work produced by H_2/O_2 cell and
- Based on the HHV (284 kmol H₂). Cross over point is 950 K.
- Comparison is not necessarily meaningful.

Open Circuit Cell Potential:

 $\hat{w}_{\text{max}} = \Delta \hat{g}_R = \Delta \mathcal{E} \zeta$ (work of moving charge ζ across a potential difference $\Delta \mathcal{E}$) $\varsigma = n_e \varsigma_e N_a = n_e \mathfrak{S}_a$

n_e: number of electrons produced when oxidizing one fuel molecule

$$
N_a = 6.023 \times 10^{23} \, mole^{-1} \, (Avogadro's number)
$$

 ζ _e = −1.602 × 10⁻¹⁹ Coulombs/electron

 $\mathfrak{S}_a = \mathfrak{S}_{e^-} N_a = 9.6485 \times 10^4$ Coulombs/mole (Faraday's number)

for the hydrogen-oxygen, $n_e = 2$, and $\zeta = 2\zeta_e$, $N_a = 2\zeta_a$,

 ω 300K, $\Delta \mathcal{E} = 1.18$ volts with water leaving in vapor form

 $\Delta \mathcal{E} = 1.23$ volts with water leaving in liquid form. For the methanol-oxygen reaction, $\Delta \mathcal{E}_o = 1.21$ *V*.

The Nernst Equation: effect of pressure and fuel concentration

$$
\Delta \mathcal{E}(p^*, T^*) = \Delta \mathcal{E}^O(T^*) - \frac{\Re T^*}{n_e \Im} \ln \left(\frac{\prod_{prod} (p_i^*)^{v_i^*}}{\prod_{real} (p_i^*)^{v_i^*}} \right) = \Delta \mathcal{E}^O(T^*) - \frac{\sigma \Re T^*}{n_e \Im_a} \ln \left(\frac{p^*}{p_o} \right) - \frac{\Re T^*}{n_e \Im_a} \ln \left(\frac{\prod_{prod} X_i^{v_i^*}}{\prod_{real} X_i^{v_i^*}} \right)
$$

\n
$$
= \Delta \mathcal{E}^O(T^*) + \Delta \mathcal{E}_P(p^*, T^*) + \Delta \mathcal{E}_{conc}(X_i, T^*) \quad \text{where } \sigma = \sum_{prod} v_i^* - \sum_{react} v_i^*
$$

\nfor a hydrogen-oxygen cell:
$$
\Delta \mathcal{E}_{conc} = \frac{\Re T^*}{2 \Im_a} \left(\ln \left(X_{H_2} \right)_{fuel} + \frac{1}{2} \ln \left(X_{O_2} \right)_{oxy} - \ln \left(X_{H_2O} \right)_{sep/fuel/oxy} \right)
$$

Equation applied at one point (under equilibrium, things are subtle). Lower reactants concentrations decrease the OC potential, especially at higher T. Using air instead of oxygen also penalizes the potential, $\Delta \bm{\mathcal{E}}_{conc, O2}$ = 2.15 $\times 10^{-5} T$ * $\ell n(0.21)$ = -0.012 @350*K*

Using products of methane reforming as fuel: $\text{CH}_4 + 2\text{H}_2\text{O} \rightarrow \text{CO}_2 + 4\text{H}_2$ $X_{\text{H}_2} = 0.8, \ \ \Delta \mathcal{E}_{conc} = 2.15 \times 10^{-5} T \cdot ln(0.8)$ this reduces the OC by $\Delta \mathcal{E}_{conc,H_2} = 0.00168V$ (@350*K*)

Impact of fuel, concentration, temperature and pressure

 P=10 thin line P=1, thick lines

 Colors for different fuel concentrations

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Impact of fuel, concentration, temperature and pressure

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Fuel Cell Components

Figure 3-1 (a) Schematic of Representative PEFC (b) Single Cell Structure of Representative PEFC(1)

Also known as membrane-electrode-assembly (MEA), and made of one "physical" plate with anode and electrode material deposited on both side.

 The membrane is a polymer (nafion) for low T cells and a ceramic plate for high T cells.

Images courtesy of DOE.

 (a)

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Electrochemical Reactions and Types of Fuel Cells

Overall Reaction: $H_2 + \frac{1}{2}O_2 \Rightarrow H_2O$ 2 (A) $H_2 \Rightarrow 2H^+ + 2e^-$ and (C) $\frac{1}{2}O_2 + 2H^+ + 2e^- \Rightarrow H_2O$, acidic electrolyte (PEM cell) $(A) H_2 + O^{2-} \Rightarrow H_2O + 2e^-$ and $(C) \frac{1}{2}O_2 + 2e^- \Rightarrow O^{2-}$ $\frac{1}{2}O_2 + 2e^- \Rightarrow O^{2-}$, alkaline electrolyte (SOFC cell) $(A) H₂ + 2OH⁻ \Rightarrow 2H₂O + 2e⁻$ and $(C) \frac{1}{2}O₂ + H₂O + 2e⁻ \Rightarrow 2OH⁻$ $\frac{1}{2}O_2 + H_2O + 2e^- \Rightarrow 2OH^-$, alkaline electrolyte (Alkaline cell with humidified air) Overall Reaction: $CO + \frac{1}{2}O_2 \Rightarrow CO_2$ $(A) CO + O^{2-} \Rightarrow CO_2 + 2e^-$ and $(C) \frac{1}{2}O_2 + 2e^- \Rightarrow O^{2-}$ $\frac{1}{2}O_2 + 2e^- \Rightarrow O^{2-}$, alkaline electrolyte (SOFC cell) Overall Reaction: $\text{CH}_4 + 2\text{O}_2 \Rightarrow \text{CO}_2 + 2\text{H}_2\text{O}$ $(A) CH_4 + 4O^2 \rightarrow CO_2 + 2H_2O + 8e^-$ and $(C) 2O_2 + 8e^- \rightarrow 4O^2$, alkaline electrolyte (SOFC cell) in all, two electrons are produced per oxygen atom.

Fuel Cell Types

Materials for Solid Oxide Fuel Cells

© PECS. All rights reserved. This content is excluded from our Creative Commons license. For more information, see<https://ocw.mit.edu/fairuse>. In the left bubble, oxygen is reduced at the cathode and oxygen ions are conducted through the electrolyte. Oxygen ions move into the anode (right bubble), where they are used to oxide the fuel at the three-phase boundary TPB). Electrons released in the charge-transfer reactions are conducted through the anode (metal), to the external circuit.

LaMnO₃ (lanthanum manganese oxide) is used to catalyze the oxygen reduction reaction on the cathode side YZS (Yittria stabilized zirconia) is use as an ion transport membrane Ni (nickel) is used to catalyze the fuel oxidation reaction on the anode side.

Solid Oxide Fuel Cells

High T cells use regular metals as catalysts

Electrolyte: YSZ, Anode: Ni-YSZ, Cathode: Sr-doped LaMnO3

YSZ = yttria – stabilized zirconia

Fuel Utilization and its impact on the Open Circuit Potential and Cell Efficiency

$$
v'_{fl} \chi_{fl} + v'_{ox} \chi_{ox} \to v''_{p} \chi_{p},
$$

$$
\Delta \mathcal{E} = \Delta \mathcal{E}^{(o)} - \frac{\sigma \mathfrak{R} T^*}{n_e \mathfrak{I}_a} ln\left(\frac{p}{p_o}\right) + \frac{\mathfrak{R} T}{n_e \mathfrak{I}_a} ln\left(\frac{X_{fl} X_{ox}^{v_o}}{X_{p}^{v_p}}\right)
$$

concentrations of fuel and oxidizer decrease between inlet and outlet as both are consumed accordignto their stoichiometric ratio

@ Inlet: $X_{f1} = \frac{1}{1 + 1}$ Partial Fuel utilization: $\varphi = \frac{n_{f11} - n_{f22}}{n_{f21}}$ $\frac{1}{1+n_{d1}}, \quad X_{ox1} = 0.21,$ ω exit: $X_{f12} = \frac{1-\varphi}{1-\varphi + n_{d1} + v_p^{\dagger}\varphi}$, $X_{ox2} = \frac{(1-\varphi)v_{ox}^{\dagger}}{3.76v_{ox}^{\dagger} + (1-\varphi)v_{ox}^{\dagger}}$

using values at exit gives lower $\Delta \mathcal{E}$

For a SOFC where products form in the fuel channel

The fuel mixture *has* $X_{H2} = 0.8$ If products of methane-water reforming are used: $CH₄ + 2H₂O \rightarrow CO₂ + 4H₂$ Oxidizer is air, X_{O2 ^{-inlet} = 0.21 Much air is flown to ensure that oxidation is not limited by oxygen Assume that @ exit, 50% utilized of oxygen, $X_{O2-exit} = 0.105$

 Open Circuit potential for different fuel utilization and for 50% oxygen utilization, cell (Fuel Cell Explained, Laramie etal.) is fueled by hydrogen produced by SMR

 There advantages to running the cell at low T, but chemistry is slow and we need a precious metal catalyst, which make it expensive and sensitive to fuel impurities.

- • In this example, products are mixed with fuel in the fuel channel, reducing the fuel concentration towards the exit.
- • Methane can also be "naturally" reformed internally, hydrogen and CO are more electro-chemically active

Fig. 3. Nemst potential for three fuels-air systems as a function of percentage of the fuel utilization. As the fuel is "utilized" it is converted to stoichiometric products that dilute the fuel on the anode side. The air is not depleted in this system.

Fuel Cell Performance at Finite Current (Power) Conditions

Faraday's Law:
$$
I = n_e \mathfrak{S}_a \dot{n}_f
$$
 or $i = n_e \mathfrak{S}_a j_f$

 Relative contributions depend on design and operating conditions:

- Catalysis, type and density.
- Thickness of electrodes and membrane.
- Water management (in PEM cells).

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