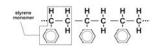
3.014 Lab $3 \gamma_2$

Phase Separation Zil Friend 11/16, 11/18 & 11/21

Lab Procedures

- Prepare Solutions
- Methylcyclohexane (Solvent)
- Polystyrene (Solute)
 - -MW = 13,200
 - -MW = 50,000
 - -MW = 29,300



polystyrene

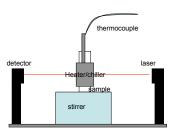


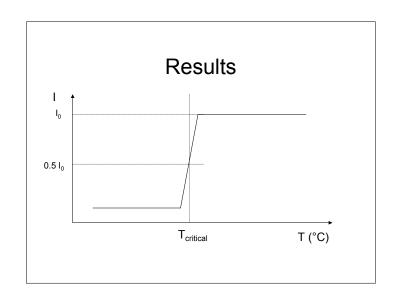
Methyl cyclohexane

 C_7H_{14}

Lab Procedures

- Temperature range: 60°- 5° C controlled by thermal cell.
- Light from laser scatters in sample cell.
- Laser signal at each T step





Lab Safety

- · Laser: Do not look into beam.
- Wear gloves & glasses when preparing & handling chemical solutions.
- Methyl cyclohexane: flammable, vapors should not be inhaled.

Review: Ideal Solution Theory

- Helmholtz Free Energy:
 - F=U-TS
 - U: Interaction energies between solution components
 - S: Entropy of mixing

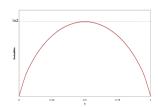
Review: Ideal Solution Theory

- S: Entropy of Mixing
- Filling N lattice sites with N_A solvent molecules & N_B solute molecules
- # states = $N!/N_A!N_B!$
- ΔS_{Mix}=k In(#states)

= - k
$$(N_{\Delta} \ln x_{\Delta} + N_{B} \ln x_{b})$$

 $\Delta S_{Mix} / kN = -x_A Inx_A - (1-x_A) In(1-x_A)$

Review: Ideal Solution Theory



- $\Delta S_{Mix} / kN = -x_A lnx_A (1-x_A) ln(1-x_A)$
- -T\Delta S term is negative for all x_A
- Mixing reduces free energy!
- Ideal case ONLY assumes no energy associated with mixing.
- What about the real world?

Review: Regular Solution Model

- · Interactions between A and B
- $U = (\#AA)E_{AA} + (\#BB)E_{BB} + (\#AB)E_{AB}$
- U=

 $(zE_{AA}/2)N_A+(zE_{BB}/2)N_B+kT\chi_{AB}(N_AN_B/N)$

- -z = #A nearest neighbors
- $-\chi_{AB}$ = Exchange parameter
- $-\chi_{AB} = (z/kT) [E_{AB-} (E_{AA} + E_{BB})/2]$

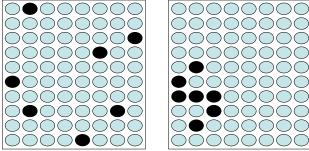
Review: Regular Solution Model

- $\Lambda F = \Lambda U T \Lambda S$
- **▲**F/NkT =

 $\mathbf{x}_{AB}(\mathbf{x}_{A})(1-\mathbf{x}_{A}) + \mathbf{x}_{A} \ln \mathbf{x}_{A} + (1-\mathbf{x}_{A}) \ln(1-\mathbf{x}_{A})$

- χ_{AB} usually >0
- · Competition between Entropy and Mixing Energy terms!
 - Entropy: Pro-Mixing
 - Energy: (often) Anti-Mixing

Polymer Solutions



Small Solute-Solvent System

Polymer-Solvent System

Polymer Solutions

- Different from regular solution model.
- · Why?
- Polymers are BIG CHAINS
- Use Flory-Huggins Model to describe polymer solutions

Flory-Huggins Model

- Need to take into account that polymers are long chains of N segments
- Each segment takes 1 lattice site
- $M = N n_p + n_s$
 - M = Total # lattice sites
 - $-n_p$, n_s = # polymers, solvent molecules

Flory-Huggins Model

- Regular Solution Energy
 $$\begin{split} \textbf{U} &= (\textbf{z}\textbf{E}_{AA}/2)\textbf{N}_{A} + (\textbf{z}\textbf{E}_{BB}/2)\textbf{N}_{B} + \textbf{k}\textbf{T}\chi_{AB}(\textbf{N}_{A}\textbf{N}_{B}/\textbf{N}) \\ &- \chi_{AB} = (\textbf{z}/\textbf{k}\textbf{T}) \left[\textbf{E}_{AB} \cdot (\textbf{E}_{AA} + \textbf{E}_{BB})/2\right] \end{split}$$
- Polymer Solution Energy
 $$\begin{split} \textbf{U} &= (z\textbf{E}_{SS}/2)\textbf{n}_S + (z\textbf{E}_{PP}/2)\textbf{N}\textbf{n}_P + \textbf{k}\textbf{T}\chi_{SP}(\textbf{N}\textbf{n}_S\textbf{n}_P/\textbf{M}) \\ &- \chi_{SP} = (z/\textbf{k}\textbf{T}) \left[\textbf{E}_{SP^-}(\textbf{E}_{SS} + \textbf{E}_{PP})/2\right] \end{split}$$

Flory-Huggins Model

Regular Solutions

$$\Delta S_{Mix} / kN = -x_A Inx_A - x_B Inx_B$$

- N = #molecules
- Polymer Solutions

$$\Delta S_{Mix} / kM = -\Phi_S \ln \Phi_S - (\Phi_P/N) \ln(\Phi_P)$$

- M = # lattice sites
- $-\Phi$ = Lattice fraction (of Solvent & Polymer)
- N = #monomer units

Flory-Huggins Model

Helmholtz Free Energy

$$\Delta F_{\text{mix}}/kT = U_{\text{mix}}/kTM - S/k$$

$$\begin{split} \Delta F_{mix}/kT &= n_{S} \ln \Phi_{S} + n_{P} \ln \Phi_{P} + (zE_{SS}/2kT)n_{S} \\ &+ (zE_{PP}/2kT)Nn_{P} + \chi_{SP}(Nn_{S}n_{P}/M) \end{split}$$

Fun with Free Energy Curves

- $(1/kT) \delta F/\delta n = \mu$
 - "chemical potential"
 - Common tangent defines 2-phase coexistance curve
- $(1/kT) \delta^2 F/\delta n^2 = 0$
 - Spinodal decomposition curve edge
- >0 ("concave" curve) phase split increases Free Energy
- <0 ("convex" curve) phase split decreases Free Energy

Fun with Free Energy Curves

- $(1/kT) \delta^2 F/\delta n^2 = (1/kT) \delta^3 F/\delta n^3$
 - Critical Point where separation first occurs